



US009224531B2

(12) **United States Patent**
Nussbaum

(10) **Patent No.:** **US 9,224,531 B2**
(45) **Date of Patent:** **Dec. 29, 2015**

(54) **POWER CONVERTER USING ORTHOGONAL SECONDARY WINDINGS**

(56) **References Cited**

U.S. PATENT DOCUMENTS

5,684,678	A	11/1997	Barrett	
6,087,921	A *	7/2000	Morrison	336/200
6,642,672	B2 *	11/2003	Hu et al.	315/276
6,930,893	B2 *	8/2005	Vinciarelli	363/17
8,502,520	B2 *	8/2013	Chandrasekaran	323/362
2009/0009729	A1	1/2009	Sakai	

FOREIGN PATENT DOCUMENTS

CN	1391334	A	1/2003
CN	1439461	A	9/2003
EP	0246377		5/1987
EP	0778659		6/1997
GB	1416403		12/1975
SU	1112505	A2	9/1984

OTHER PUBLICATIONS

Jitaru, Ionel Dan. "Signal Transfer Through Power Magnetics." 2002 Power Technology Symposium. IBM Power Technology and Qualifications. , Bloomington, Minnesota. (Sep. 2002). 6 pgs.
International Search Report and Written Opinion dated Mar. 28, 2013 for PCT/US2010/029651.

* cited by examiner

Primary Examiner — Adolf Berhane

Assistant Examiner — Afework Demisse

(57) **ABSTRACT**

A power conversion device includes a magnetic core; and a plurality of windings surrounding portions of the magnetic core, including a first set of windings defining a first magnetic flux path, a second set of windings defining a second magnetic flux path magnetically orthogonal to the first magnetic flux path, and a third set of windings. Each winding of the third set of windings is configured to be excitable via both the first flux path and the second flux path.

17 Claims, 8 Drawing Sheets

(75) Inventor: **Michael Nussbaum**, Newton, MA (US)

(73) Assignee: **BOSE CORPORATION**, Framingham, MA (US)

(*) Notice: Subject to any disclaimer, the term of this patent is extended or adjusted under 35 U.S.C. 154(b) by 1244 days.

(21) Appl. No.: **13/076,923**

(22) Filed: **Mar. 31, 2011**

(65) **Prior Publication Data**

US 2012/0249105 A1 Oct. 4, 2012

(51) **Int. Cl.**

G05F 1/00 (2006.01)

H01F 27/28 (2006.01)

H02M 3/158 (2006.01)

H02M 3/335 (2006.01)

H02M 1/00 (2007.01)

(52) **U.S. Cl.**

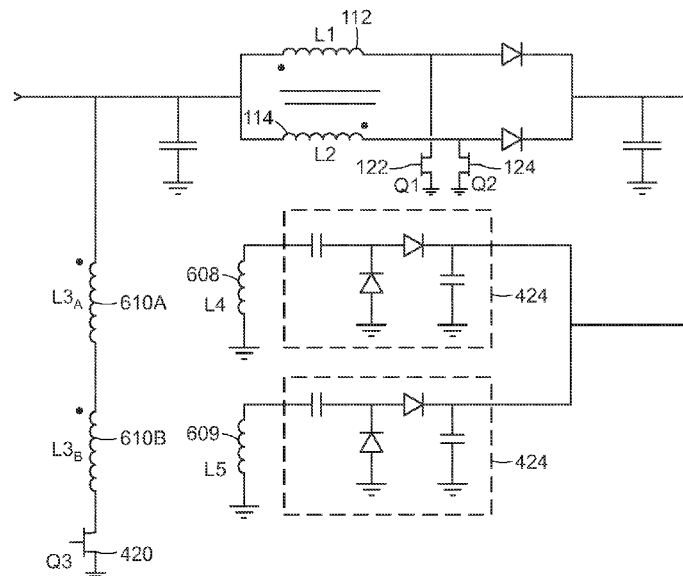
CPC **H01F 27/2804** (2013.01); **H02M 3/1584** (2013.01); **H01F 2027/2819** (2013.01); **H02M 3/33523** (2013.01); **H02M 2001/0032** (2013.01); **H02M 2001/0064** (2013.01); **H02M 2003/1586** (2013.01); **Y02B 70/16** (2013.01)

(58) **Field of Classification Search**

CPC H02M 3/1584; H02M 3/33523; H02M 2001/0032

USPC 323/213, 222, 232, 247, 250, 262, 172, 323/282, 301, 332, 334; 336/200, 214, 221, 336/232, 233

See application file for complete search history.



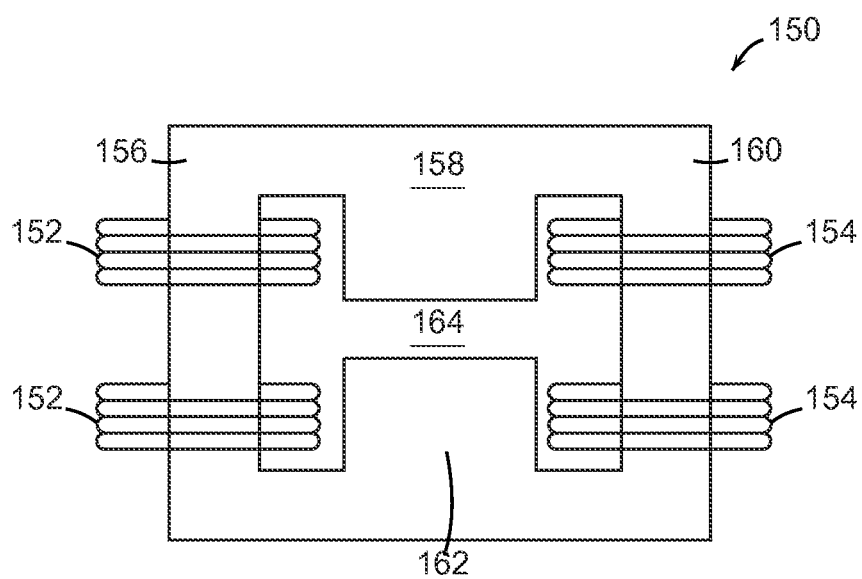


FIG.1A
(Prior Art)

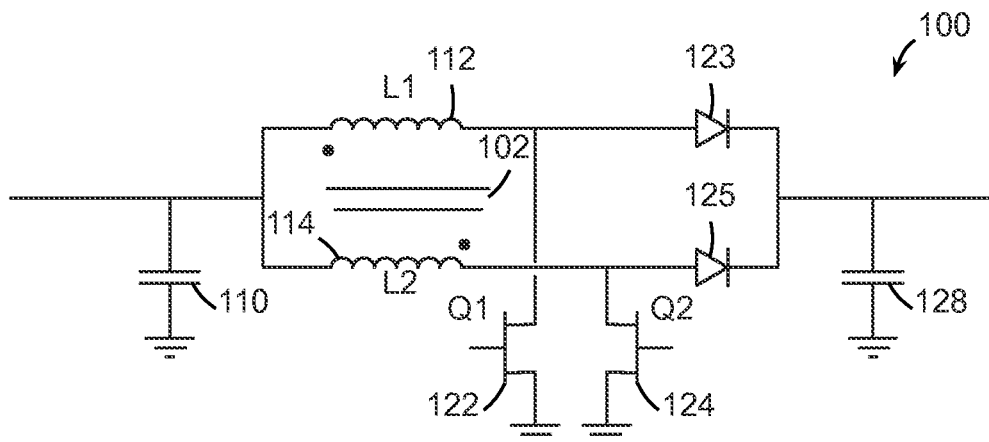


FIG. 1B
(Prior Art)

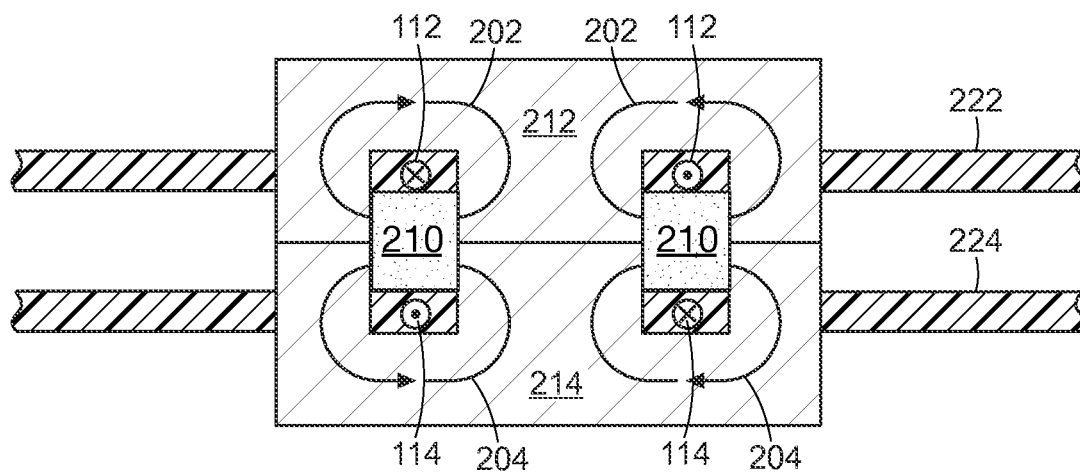


FIG. 2

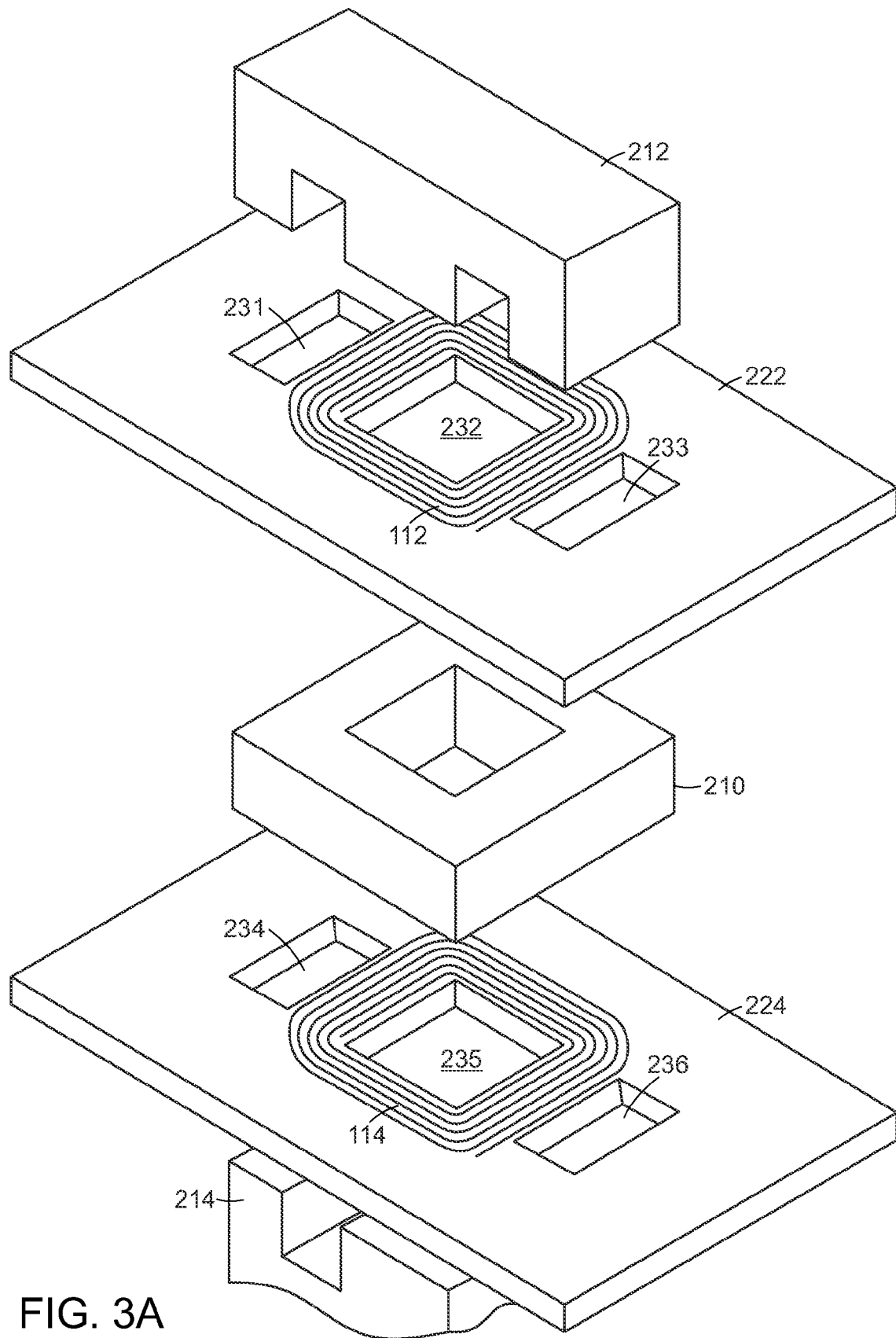


FIG. 3A

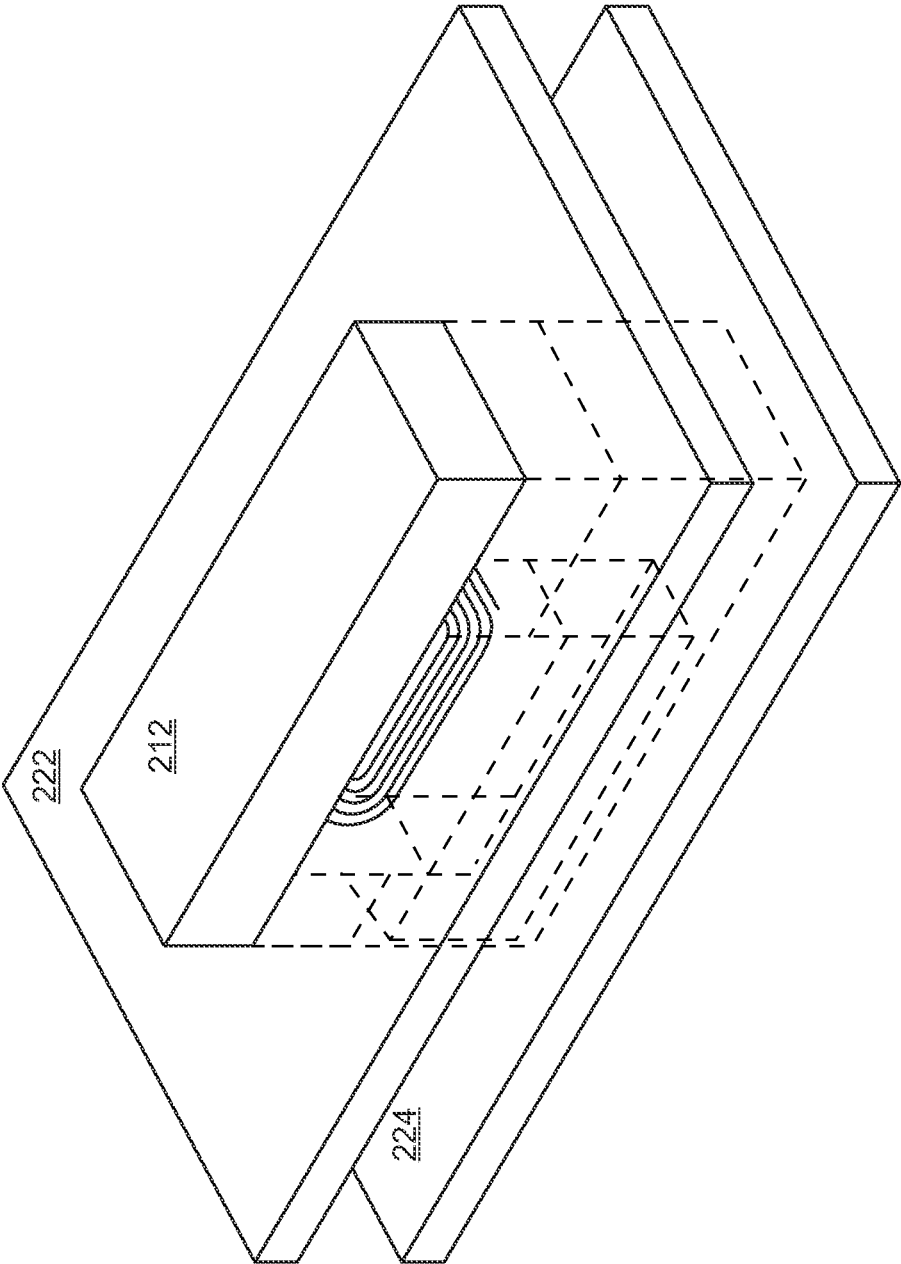


FIG. 3B

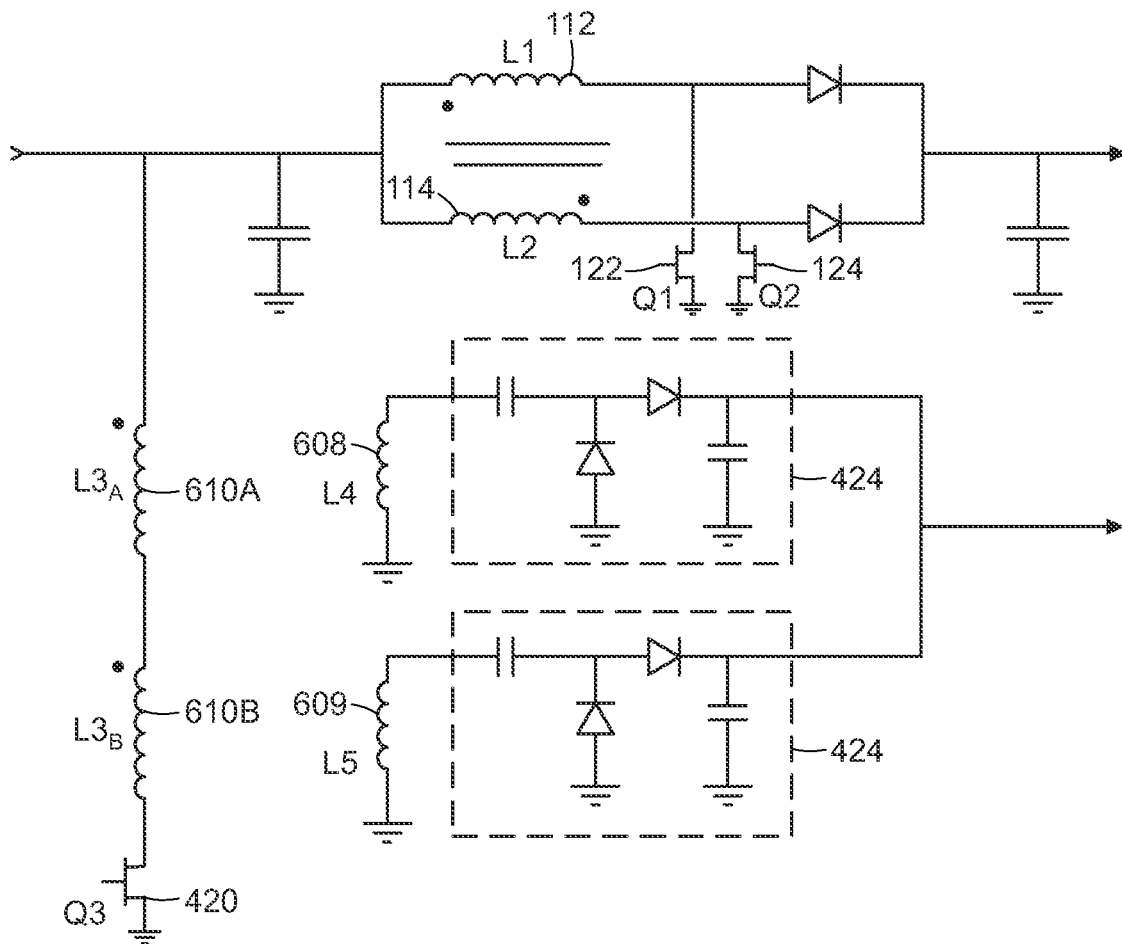


FIG. 4

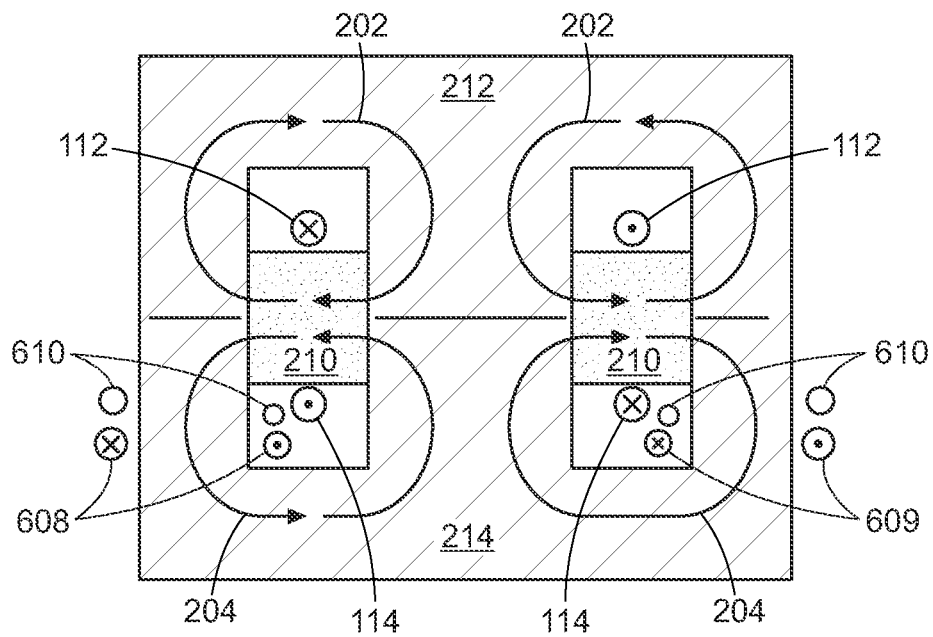


FIG. 5A

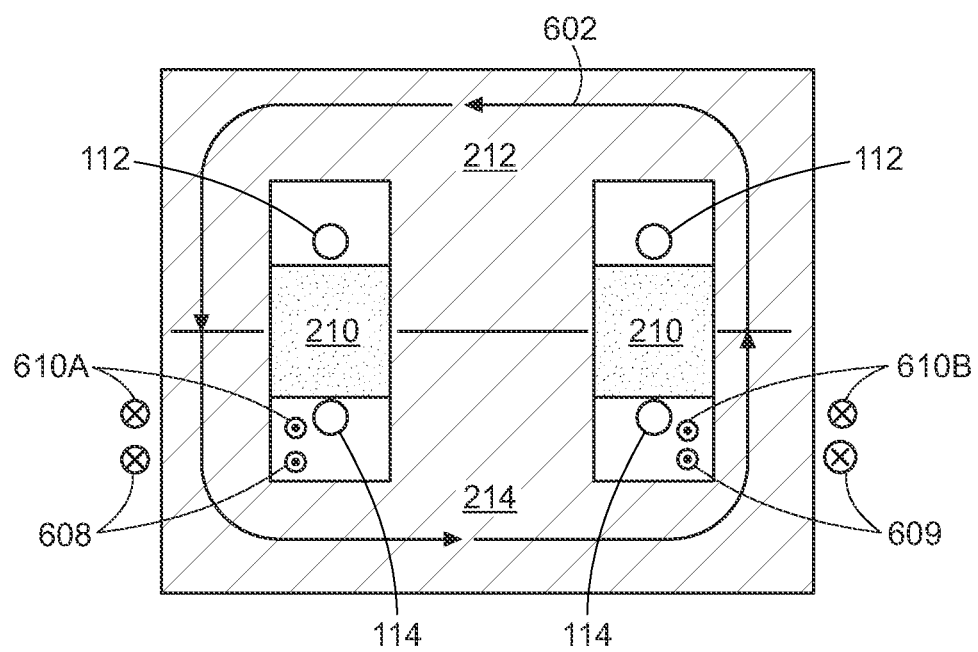


FIG. 5B

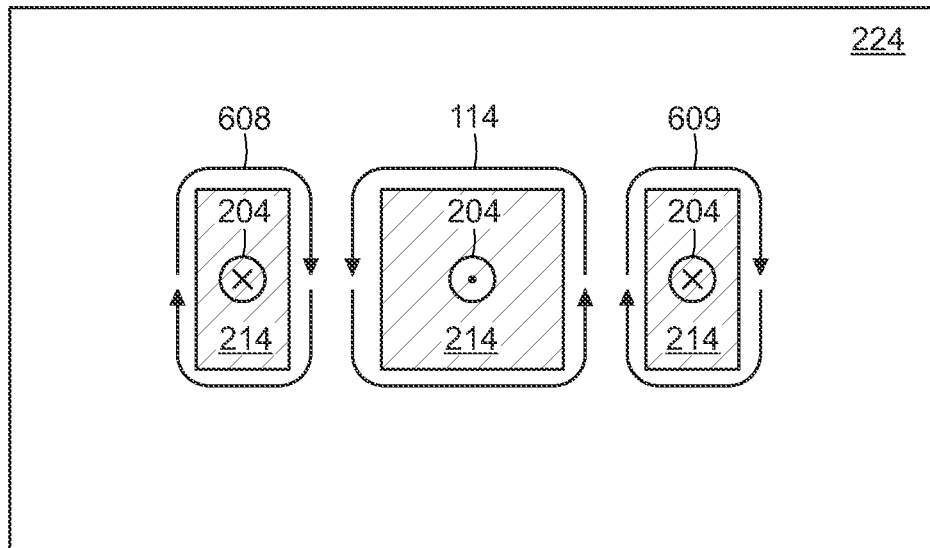


FIG. 6A

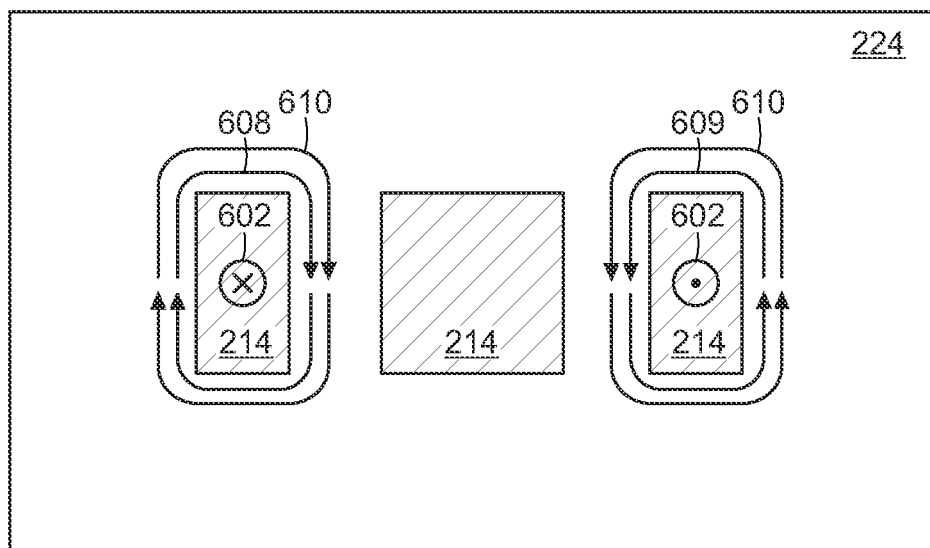


FIG. 6B

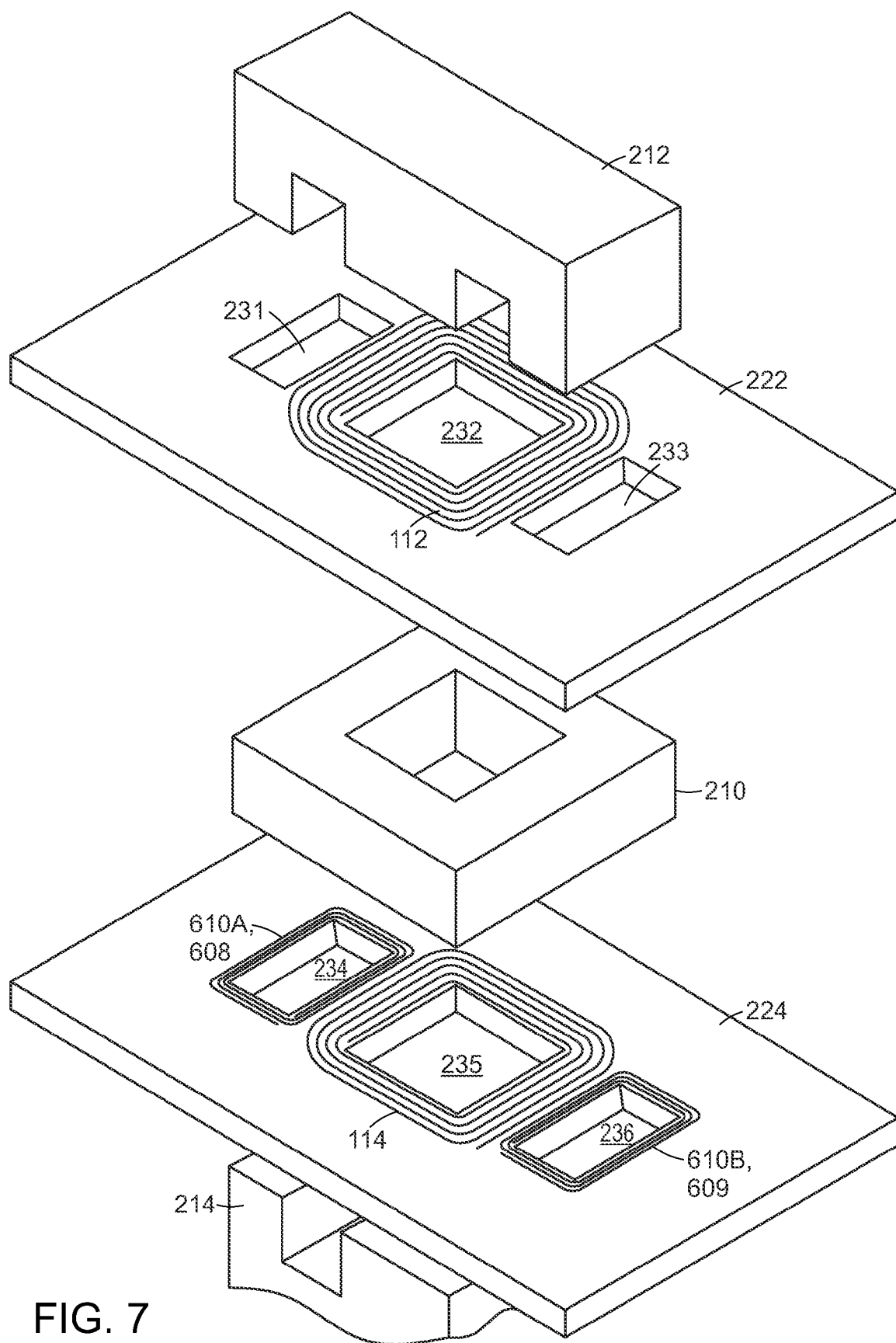


FIG. 7

1

POWER CONVERTER USING ORTHOGONAL SECONDARY WINDINGS

CROSS-REFERENCE TO RELATED APPLICATIONS

This application claims priority to U.S. application Ser. No. 13/076,923, filed on Mar. 31, 2011, titled "POWER CONVERTER USING SOFT COMPOSITE MAGNETIC STRUCTURE" and filed concurrently with the present application, which is incorporated herein by reference.

BACKGROUND

Some power conversion systems, for example, dual interleaved boost power factor converter (PFC) systems, make use of magnetically coupled inductors or coils wound around a magnetic core. For instance, referring to FIG. 1A, a magnetic core **150** of a boost converter includes a first set of inductor coils **152** and a second set of inductor coils **154**. Inductor coils **152** are disposed around a first leg **156** of a core **158**, and inductor coils **154** are disposed around a second leg **160** of the core. Energy storage in boost converter **150** is localized in a center leg **162** including a gap **164**. The magnetic (H) field in gap **164** is oriented perpendicular to the wide axis of inductor coils **152** and **154**. Boost converters including magnetic core **150** are generally suitable for a power throughput of about a few hundred Watts. However, attempts to scale up such boost converters may face efficiency limitations in some systems, for instance due to geometry constraints and/or eddy current losses when the power rating is increased beyond the 1 kW range. In some examples, the power conversion systems are used in professional sound systems.

Some power conversion systems make use of one primary winding and multiple secondary windings, with one of the secondary windings being used to provide "housekeeping" power to control circuitry, such that a separate power conversion component is not needed to power the control circuitry. In situations in which the control circuitry requires power during standby periods, the production of housekeeping power may be inefficient, for example, due to losses in the switching components of the system driven by the primary windings. This inefficiency negates some of the advantages of sharing the primary windings for multiple sets of secondary windings during normal operation.

Referring to FIG. 1B, an example of a dual interleaved boost converter circuit **100** includes inductors **L1 112** and **L2 114**, which are magnetically coupled across a common core **102**. The degree of coupling between the inductors is controlled by the width of the gap separating the windings of the two inductors. The maximum flux ripple in the core of the dual interleaved boost converter circuit **100** is roughly half that of a single boost circuit, and the AC ripple on the dual interleaved boost circuit is also reduced. Two switches **Q1 122** and **Q2 124** (e.g., metal-oxide-semiconductor field effect transistors (MOSFETs)) are duty cycle controlled and typically run 180° out of phase, although in some cases 90° operation may be preferable. A circuit having sufficiently coupled inductors exhibits little to no ripple current.

SUMMARY

In a general aspect, a power conversion device includes a magnetic core; and a plurality of windings surrounding portions of the magnetic core, including a first set of windings defining a first magnetic flux path, a second set of windings defining a second magnetic flux path magnetically orthogonal

2

to the first magnetic flux path, and a third set of windings. Each winding of the third set of windings is configured to be excitable via both the first flux path and the second flux path.

Embodiments may include one or more of the following.

5 The device is operable in a plurality of modes, including a first mode in which power is transferred from one or more windings of the first set of windings to the windings of the third set of windings, and in a second mode in which power is transferred from windings of the second set of windings to the windings of the third set of windings.

10 The device further includes circuitry to form a first power supply using the first set of windings operable only in the first mode, and circuitry to form a second power supply for providing power via the third set of windings operable in both the first mode and the second mode.

15 The first mode comprises a primary operating mode and the second mode comprises a standby operating mode. The first power supply has a power capacity as least ten times greater than the second power supply. The first power supply has a power capacity of at least 0.2 kW.

20 The first power supply comprises a boost converter. The first set of winding comprises a plurality of windings coupled by the magnetic core, and wherein the boost converter comprises an interleaved boost converter.

25 The circuitry further comprises a rectifier coupled to each of the winding of the third set of windings. The circuitry further comprises a charge pump coupled to each of the winding of the third set of windings.

30 The second set of windings comprises a plurality of windings arranged in a serial connection, and the third set of windings comprises a plurality of windings. Each winding of the third set of windings corresponds to a different one of the windings of the second set of windings.

35 Each of the windings of the first set of magnetic windings is coupled to a MOSFET having a first current rating, and wherein each winding of the second set of windings is coupled to a MOSFET having a second current rating less than the first current rating.

40 Each winding of the first set of winding is disposed on a substrate of a set of one or more substrates, the magnetic core passing through openings in the substrates.

45 In another general aspect, a method for power conversion includes, in a first operating mode, exciting windings of a first set of windings surrounding portions of a magnetic core causing a first power output. The exciting of the first set of windings causing a second power output via a third set of windings magnetically coupled to the first set of windings via the magnetic core. The method further includes, in a second operating mode, exciting winding of a second set of windings surrounding portions of the magnetic core, a second magnetic flux path formed by the second set of windings being magnetically orthogonal to a first magnetic flux path formed by the first set of windings. The exciting of the second set of windings causing a power output via the third set of windings magnetically coupled to the second set of windings via the magnetic core.

50 Embodiments may include one or more of the following.

55 The first operating mode comprises a primary operating mode and the second operating mode comprises a standby operating mode.

60 The first set of windings form part of a first power supply and the second set of windings form part of a second power supply. The first power supply has a power capacity at least ten times greater than the second power supply.

65 In a general aspect, a power conversion device includes a magnetic core; and a plurality of windings surrounding portions of the magnetic core, including a first winding and a second winding magnetically coupled through the magnetic

3

core. The magnetic core comprises a first part formed of a first material and a second part formed of a second material, the first material having a first stiffness and the second material having a second stiffness substantially less than the first stiffness. The first winding and the second winding are magnetically coupled through the first part of the magnetic core.

Embodiments may include one or more of the following.

The first material has a first magnetic permeability and the second magnetic material has a second magnetic permeability less than the first magnetic permeability.

The first material comprises ferrite.

The second material comprises a composite. The second material includes a polymer. The second material includes at least one of iron powder, ferrite powder, Sendust, Metglass powder, or an amorphous soft magnetic alloy.

The second stiffness is about 1000 times less than the first stiffness. The second stiffness is less than about 100 MPa.

The first winding is disposed on a first substrate and the second winding is disposed on a second substrate, the magnetic core passing through openings in the first substrate and the second substrate.

The first part of the magnetic core comprises a first element and a second element. The first element includes a plurality of first legs, each first leg configured to fit through a corresponding opening in the first substrate. The second element includes a plurality of second legs, each second leg configured to fit through a corresponding opening in the second substrate. The first legs and the second legs mate to form the first part of the magnetic core.

The first substrate is a first circuit board and the second substrate is a second circuit board.

The second part of the magnetic core comprises a third element, the third element coupled in contact with the first part of the magnetic core. At least a portion of the third element is disposed between the first winding and the second winding.

The second part of the magnetic core forms an annular structure.

The device further includes circuitry coupled to the windings forming a power converter. The first winding and the second winding form coupled inductors. The power converter comprises a dual interleaved boost converter. During operation of the boost converter, the first winding and the second winding form coupled inductors and during operation cyclical energy storage in the magnetic core is substantially concentrated in the second part of the magnetic core.

In another general aspect, a method for assembling a power conversion device includes assembling a magnetic core having a first part formed of a first material and a second part formed of a second material, the first material having a first stiffness and the second material having a second stiffness substantially less than the first stiffness. Assembling the magnetic core includes disposing a first element of the first part of the core within a first winding; and forming the second part of the core to maintain contact with the first part of the core such that the second part of the core forming at least part of magnetic flux paths induced by current in the first winding.

Embodiments may include one or more of the following.

The first material has a first magnetic permeability and the second material has a second magnetic permeability less than the first magnetic permeability.

The method further includes disposing a second element of the first part of the core within a second winding. The second part of the core providing magnetic coupling between the first winding and the second winding. The method further includes mating the first element and the second element of

4

the first part of the core; and forming the second part to maintain contact with the first part after mating the first and the second elements.

The first winding is formed on a first substrate, and wherein disposing the first element of the first part of the core within a first winding includes passing the first element through one or more openings in the first substrate.

The second part comprises a mechanically soft material, and forming the second part to maintain contact with the first part includes deforming the second part.

Forming the second part to maintain contact with the first part includes positioning a precursor of the second material in a region defined at least in part by the first part of the core; and causing a transformation of the precursor material to form the second material. Causing the transformation comprises curing the precursor material. The precursor material comprises a liquid material, and wherein position the precursor comprises pouring the precursor into the region.

Among other advantages, the systems and methods described herein provide a scalable geometry that allows a dual interleaved boost converter to operate at the multi-kW level without significant AC conductor losses. In general, a system having coupled inductors has low core losses due to a reduced AC flux component in the core, and a smoother current and less loss in switches due to a reduced RMS current flowing in the switches.

The use of a material in the boost converter that is both magnetically and mechanically soft allows strict manufacturing tolerances to be achieved without a gap between materials and without the generation of thermal stresses or cracks. In some cases, the boost converter can be fabricated at room temperature, allowing the fabrication process to be readily integrated with existing manufacturing processes.

A boost converter having the ability to generate standby power without driving the large loads coupled to the main primary induction coils reduces switching losses and other power inefficiencies.

Other features and advantages of the invention are apparent from the following description and from the claims.

BRIEF DESCRIPTION OF DRAWINGS

FIG. 1A is a side cross-sectional view of a boost converter.

FIG. 1B is a circuit diagram of a dual interleaved boost circuit.

FIG. 2 is a side cross-sectional view of a boost converter having a magnetic core formed from two materials.

FIGS. 3A and 3B are perspective views of the boost converter of FIG. 2 as exploded and as assembled, respectively.

FIG. 4 is a circuit diagram of a boost circuit with low-power windings.

FIGS. 5A and 5B are side cross-sectional views of a boost converted with coils for low power driven by main power coils and driven by low power coils, respectively.

FIGS. 6A and 6B are top cross-sectional views of the boost converters shown in FIGS. 5A and 5B, respectively.

FIG. 7 is a perspective view of a boost converter configured for normal and standby operation.

DETAILED DESCRIPTION

Referring to FIGS. 2 and 3A-B, in some embodiments, the dual interleaved boost circuit 100 shown in FIG. 1 is implemented using a magnetic core made up of multiple elements 210, 212, 214 that are assembled together surrounding the windings 112, 114 of the inductors. Winding 112 is formed on a printed circuit board 222 around a central opening 232 of the

board. Winding **114** is similarly formed around a central opening **235** of a second printed circuit board **224**. As shown in the exploded view of FIG. 3A, the magnetic core is formed in part by a first multi-legged element **212**, the legs of which, when assembled as shown in FIG. 3B, pass through openings **231**, **232**, **233** in the first circuit board **222**. The magnetic core is further formed by a second multi-legged element **214**, the legs of which, when assembled, pass through openings **234**, **235**, **236** in the second circuit board **224** such that the legs of elements **212** and **214** mate between the two printed circuit boards. When assembled, each of the windings **112**, **114** is effectively wound around the mated center legs of the first and second elements **212**, **214**. As shown in the cross-sectional view of FIG. 2, the mated first and second elements **212**, **214** do not fill the area between the windings.

In general, elements **212** and **214** are made of a material with a high magnetic permeability (relative permeability μ), such as ferrite, to enable magnetic coupling between the windings. In the area between the windings, a low- μ material allows for energy storage, which is proportional to μ^{-1} . In some embodiments, the magnetic core is further formed from a third element **210** of a different material than the first two elements. Referring to FIG. 3A, in some embodiments, this third element **210** forms a ring or “donut” shape (e.g., a rectangular ring or a substantially circular ring) such that, when assembled, the third element fills the space between the windings where the air gap would have been.

In some cases, the material of the third element **210** has a significantly lower magnetic permeability μ (i.e., higher magnetic reluctivity) than the first **212** and second **214** elements. Referring again to the cross-sectional view of FIG. 2, the magnetic field lines **202**, **204** induced by corresponding currents in the windings **112**, **114** are largely coupled via the high-permeability elements **212**, **214**, while energy storage is primarily localized to the lower-permeability ring element **210**.

In some embodiments, the first and the second core elements **212**, **214** are formed of a mechanically hard, magnetically soft material, such as ferrite (which has an elastic modulus of about 100 GPa). These parts may be difficult to manufacture to high dimensional tolerance or to maintain at a precise dimension due to environmental factors (e.g., temperature). For example, the lateral distance between the legs of the elements may not be fabricated to a predictable precise dimension.

In some embodiments, the third ring element **210** of the core is formed from a mechanically soft material having an elastic modulus of about 1000 times less than the elastic modulus of the rigid material of the first and second core elements. For instance, in some embodiments, the modulus of the third ring element is limited to no more than about 100 MPa. An example of a suitable type of material is a soft, pliable composite combining a magnetic phase (e.g., iron powder, ferrite powder, Sendust, or another finely ground magnetically soft material capable of providing low hysteresis and eddy current losses) in a polymer matrix (e.g., a rubber, an epoxy, or a urethane). The third ring element has a magnetic permeability in the range of about 8-80, or preferably in the range of about 10-30. One example of such a material, made by Daido Steel Co., Ltd. (Tokyo, Japan), is a composite of a Metglas® alloy (Metglas, Inc., Conway, S.C.) in a rubber matrix that exhibits AC losses close to that of powdered iron ($\mu=10$) and has a permeability $\mu=30$ at zero field.

In general, the mechanically hard components (i.e., circuit boards **222**, **224** and hard elements **212**, **214** of the core) are assembled using standard manufacturing processes. In some

embodiments, the components are assembled leaving a gap into which ring element **210** can later be inserted rather than the ring being inserted during initial assembly. In some embodiments, an uncured precursor to the material of ring element **210** is squeezed into the gap and cured at elevated temperature to form the ring element. In other embodiments, ring element **210** is formed outside of the boost converter and mechanically deformed as it is pushed into the gap or as the other elements of the boost converter are pushed around the ring element. In some examples, the ring element **210** is formed of a putty-like material. To be compatible with existing manufacturing protocols, room temperature fabrication and assembly of boost converter, including insertion of third element **210** of the core, is preferable.

In some examples, the third element **210** is formed from a material that cures during or after the manufacturing process. For example, the material may be soft during assembly and then hardened in a curing process. In general, even in its hardened state, the material of the third element remains mechanically softer (e.g., about 1000 times softer) than the material of the mechanically hard elements of the core) so that any strain resulting from unequal coefficients of thermal expansion is absorbed by the third element. In some examples, the material is resilient, thereby maintaining contact with the other elements of the core in the face of mechanical movement or thermal expansion of the elements. In some examples, a chamber is formed between the circuit boards, and the third element is formed by pouring or injecting a liquid into the chamber, which may then be cured to form a flexible or rigid third element. In some examples, the manufacturing process is performed at a high temperature at which the third element is soft (e.g., flexible, resilient), while in operation the device operates at a lower temperature at which the element is relatively harder (e.g., less flexible or resilient).

In other examples, the third ring element **210** of the core may be formed from a rigid material. However, if the first and second core elements are not precisely dimensioned or if the third element exhibits different thermal expansion characteristics than the first and second elements, a rigid third element may have to be under-sized sufficiently to allow assembly. Such under-sizing may result in an undesirable air gap. Furthermore, if the ring element **210** were formed of a rigid material having a substantially different coefficient of thermal expansion than that of the other elements, cracking or distortion may occur upon heating of the boost converter.

Referring to FIG. 3A, the windings of the boost converter are formed using printed circuit tracings on the printed circuit board (e.g., board **222**). For instance, the windings can include spiral paths on one or more layers of the board with the paths surrounding openings in the board through which the magnetic core passes when assembled. Note that the vertical dimension of trace is very small as compared to its horizontal dimension, thereby forming a ribbon-like conductor. In certain modes of operation, such a low vertical dimension combined with the direction of magnetic field lines reduces eddy current losses as compared to other configurations. In part, the reduced losses are due to the orientation of the magnetic field in the windings: the magnetic field (H) vector is parallel to the wide axis of the windings. The reduced losses are also due to the magnetic permeability of the winding material: the magnetic (H) field is about ten times lower in a material with $\mu=10$ than in air, and eddy current losses scale as the magnetic field squared (H^2).

The boost converter of FIGS. 2 and 3A-B may provide for reduced AC conductor losses, such as eddy current losses, as compared to a boost converter having an air gap, for instance by roughly a factor of 5, under the same operating conditions.

This reduction in AC conductor loss may bring the AC conductor loss closer to the level of the DC loss (e.g., roughly twice the DC loss), which may be desirable in many applications.

In a power factor converter (PFC) such as the boost converters described above, the PFC windings provide a high level of power to a load. For instance, the PFC windings in boost converter **100** (FIG. 1) are coupled to a pair of large MOSFET switches **122**, **124** (Q1 and Q2) which enable the PFC windings to throughput kilowatts of power.

When a PFC is delivering little or no power to the load, it may in some cases still be desirable to maintain a low level of power for standby operation. A set of secondary windings may be used to provide low power, enabling standby operation. However, driving the smaller secondary windings using the voltage across the larger primary windings (i.e., main primary windings **112**, **114**) may entail significant switching losses resulting from the drain-source capacitance of the large MOSFET switches **122**, **124** (Q1 and Q2) coupled to the primary windings.

Referring to FIG. 7, a PFC choke **600** includes three sets of windings: main primary windings L1 **112** and L2 **114**, which function as described above; secondary windings L4 **608** and L5 **609**; and primary low-power windings L3A **610A** and L3B **610B**. Secondary windings **608**, **609** and primary low-power windings **610A**, **610B** are wound around outer legs **702**, **704** of a core **700**. Secondary windings **608**, **609** provide efficient low-power output (e.g., housekeeping power) in both normal and standby operating mode, and can be excited either by currents in the main primary windings **112**, **114** (e.g., during normal operating mode) or by currents in the primary low-power windings **610A**, **610B** (e.g., during standby operation). In some embodiments, main primary windings **112**, **114** have a power capacity at least ten times greater than the power capacity of main low-power windings **610A**, **610B**, e.g., a power capacity of at least 0.2 kW.

Referring to FIGS. 5A and 6A, magnetic flux lines **202**, **204** are created by a current through main primary windings **112**, **114** (the arrows in FIG. 6A indicate the direction of current flow in the windings). Flux lines **202**, **204** are capable of exciting secondary windings **608**, **609**, e.g., during normal operating mode. Notably, flux lines **202**, **204** induce an electromagnetic field in primary low-power winding **610A** that is out of phase from the electromagnetic field induced in primary low-power winding **610B**, such that the overall field cancels and no net voltage is induced across the primary low-power windings. That is, main primary windings **112**, **114** are incapable of exciting a current in primary low-power windings **610A**, **610B**.

Referring now to FIGS. 5B and 6B, a magnetic flux path **602** is created by a current through primary low-power windings **610A**, **610B**. Flux path **602** is capable of exciting secondary windings **608**, **609**, e.g., during standby operation. Notably, none of the flux associated with primary low-power windings **610A**, **610B** links main primary windings **112**, **114**. That is, primary low-power windings **610A**, **610B** are incapable of exciting a current in main primary windings **112**, **114**.

Main primary windings **112**, **114** and primary low-power windings **610A**, **610B** are thus magnetically orthogonal to each other. That is, there is no magnetic coupling between these two sets of windings, and each set of windings can be operated independently without inducing currents in the other set of windings.

Referring FIG. 4, in the circuit of PFC choke **600**, secondary windings L4 **608** and L5 **609** are coupled through rectifier circuits **424** (e.g., a voltage double rectifier) to provide a low

voltage output. Generally, in a normal operating mode, these low power windings are coupled to and receive power from the main primary inductor windings L1 **112** and L2 **114**, as described above. In standby mode, the main windings are not energized and the secondary windings L4 **608** and L5 **609** receive power from primary low-power windings L3A **610A** and L3B **610B**, which are connected in series and coupled to a MOSFET switch **420** (Q3). That is, while the secondary windings **608**, **609** are rectified separately from the main primary windings **112**, **114** and from the primary low-power windings **610A**, **610B**, the secondary windings can be excited either by currents in the main primary windings **112**, **114** or by currents in the primary low-power windings **610A**, **610B**, depending on the operating mode.

Because Q3 (the switch coupled to primary low-power windings **610A**, **610B**) is significantly smaller than Q1 and Q2 (of the switches **122**, **124** coupled to the main primary windings), driving the secondary windings with the primary low-power windings during standby mode avoids the inefficiencies inherent in unnecessarily driving the large loads (Q1 and Q2) coupled to the main primary windings.

The use of a soft magnetic material, such as a magnetic composite, and the orthogonality of primary and secondary magnetic windings are not limited to use in PFC converter systems, but may be used generally in, e.g., any power converter system or transformer having coupled inductor windings.

It is to be understood that the foregoing description is intended to illustrate and not to limit the scope of the invention, which is defined by the scope of the appended claims. Other embodiments are within the scope of the following claims.

What is claimed is:

1. A power conversion device comprising:

a magnetic core having first, second, and third legs, the first leg being between the second and third legs; and
a plurality of windings surrounding portions of the magnetic core, including a first set of windings around the first leg and defining a first magnetic flux path, a second set of windings around the second and third legs and defining a second magnetic flux path, and a third set of windings around the second and third legs;

wherein magnetic flux in both the first magnetic flux path and the second magnetic flux path induces a current in each winding of the third set of windings, and

the first set of windings are magnetically orthogonal to the second set of windings, such that magnetic flux in the first magnetic flux path does not induce current in the second set of windings and magnetic flux in the second magnetic flux path does not induce current in the first set of windings.

2. The power conversion device of claim 1 operable in a plurality of modes, including a first mode in which power is transferred from one or more windings of the first set of windings to the windings of the third set of windings, and in a second mode in which power is transferred from windings of the second set of windings to the windings of the third set of windings.

3. The power conversion device of claim 2 further comprising circuitry to form a first power supply using the first set of windings operable only in the first mode, and circuitry to form a second power supply for providing power via the third set of windings operable in both the first mode and the second mode.

4. The power conversion device of claim 3 wherein the first mode comprises a primary operating mode and the second mode comprises a standby operating mode.

9

5. The power conversion device of claim 3 wherein the first power supply has a power capacity at least ten times greater than the second power supply.

6. The power conversion device of claim 3 wherein the first power supply has a power capacity of at least 0.2 kW.

7. The power conversion device of claim 3 wherein the first power supply comprises a boost converter.

8. The power conversion device of claim 7 wherein the first set of windings comprises a plurality of windings coupled by the magnetic core, and wherein the boost converter comprises an interleaved boost converter.

9. The power conversion device of claim 3, wherein the circuitry further comprises a rectifier coupled to each of the windings of the third set of windings.

10. The power conversion device of claim 3, wherein the circuitry further comprises a charge pump coupled to each of the windings of the third set of windings.

11. The power conversion device of claim 1 wherein the second set of windings comprises a plurality of windings arranged in a serial connection, and the third set of windings comprises a plurality of windings, each winding of the third set of windings correspond to a different one of the windings of the second set of windings.

12. The power conversion device of claim 1, wherein each of the windings of the first set of magnetic windings is coupled to a MOSFET having a first current rating, and wherein each winding of the second set of windings is coupled to a MOSFET having a second current rating less than the first current rating.

13. The power conversion device of claim 1, wherein each winding of the first set of windings is disposed on a substrate of a set of one or more substrates, the first leg of the magnetic core passing through openings in the substrates on which the first set of windings is disposed.

10

14. A method for power conversion comprising:

in a first operating mode,

providing current through windings of a first set of windings surrounding a first leg of a magnetic core, forming a first magnetic flux path,

wherein the first magnetic flux path couples power from the first set of windings to a third set of windings surrounding second and third legs of the magnetic core and magnetically coupled to the first set of windings via the magnetic core, causing a first power output from the third set of windings; and

in a second operating mode,

providing current through windings of a second set of windings surrounding the second and third legs of the magnetic core, forming a second magnetic flux path, the second set of windings being magnetically orthogonal to the first set of windings,

wherein the second magnetic flux path couples power from the second set of windings to the third set of windings magnetically coupled to the second set of windings via the magnetic core, causing a second power output from the third set of windings.

15. The method of claim 14, wherein the first operating mode comprises a primary operating mode and the second operating mode comprises a standby operating mode.

16. The method of claim 14, wherein the first set of windings form part of a first power supply and the second set of windings form part of a second power supply.

17. The method of claim 16, wherein the first power supply has a power capacity at least ten times greater than the second power supply.

* * * * *